

## **BEFORE THE FLORIDA PUBLIC SERVICE COMMISSION**

In re: Investigation into pricing of unbundled network elements

Docket No. 990649A-TP

## **AT&T COMMUNICATIONS OF THE SOUTHERN STATES, INC. AND MCI WORLDCOM, INC.'S JOINT RESPONSES TO FPSC STAFF'S THIRD SET OF INTERROGATORIES**

AT&T Communications of the Southern States, Inc. ("AT&T") and MCI WorldCom, Inc. ("MCI"), pursuant to Rule 28-106.206, Florida Administrative Code and Rules 1.350 and 1.280, Florida Rules of Civil Procedure, hereby submit the following Responses to FPSC Staff's Third Set of Interrogatories to AT&T and MCI.

INTERROGATORY NO. 22: Please refer to page 5, lines 16-19 of AT&T/WorldCom witness Donovan's supplemental rebuttal testimony filed February 11, 2002. Please identify any and all documents that support your assertion that a realistic engineer-to-technician "span of control" is 1-to-6.

**AT&T/MCI's Response:** As indicated in the relevant passage of Mr. Donovan's testimony, the 1 engineer to 6 outside plant technicians "span of control" is based on Mr. Donovan's 30+ years of telecommunications experience, not on published documents. It may be noted that BellSouth's embedded costs indicate as much as a 1 to 5.2 "span of control".

INTERROGATORY NO. 23: Referring to AT&T/WorldCom witness Donovan's supplemental rebuttal testimony filed February 11, 2002, page 9, lines 14-15, please identify all reports, studies and documents that support that a smaller manhole cannot cost more than a larger manhole.

1

This claim of confidentiality was filed by or on behalf of a "telco" for Confidential DN <u>O24399002</u>. The document is in locked storage pending advice on håndling. To access the material, your name must be on the CASR. If undocketed, your division director must obtain written EXD/Tech permission before you can access it.

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AT&T/MCI's Response: Mr. Donovan's testimony does not state that an aberrant or inefficiently purchased smaller manhole could not ever cost more than a larger manhole – just that such a pricing structure is illogical, based on his 30+ years of hands-on telecommunications experience. His opinion is not based on published documents. As indicated in Mr. Donovan's Attachment JCD-10, manholes normally consist of precast concrete (cement). The cost of such structures are generally related to the amount of concrete, the number of steel reinforcing rods embedded in the concrete, and appropriate attached hardware. The difference between a smaller manhole and a larger manhole is simply that larger manholes are made with more concrete and more steel reinforcing rods. Manholes are certainly not high tech, such that miniaturization costs more. All are heavy, bulky, and low tech. Therefore, it is simply illogical that such low tech outside plant items cost as much as BellSouth claims, and it is illogical to accept that a smaller size manhole should cost more that a manhole more than twice its size. Exhibit JCD-10 indicates the amount of reinforced concrete by weight for various sized manholes. An additional diagram is being provided as an attachment to this response to provide the approximate weight of a 224 cubic-foot manhole. Weights, which should be proportional to cost are as follows:

| Exhibit No. | Dimensions         | Cubic Feet  | Weight      | BellSouth Claim        |
|-------------|--------------------|-------------|-------------|------------------------|
| JCD-10.2    | 3' x 5' x 3'       | 45 cu. ft.  | 4,379 lbs.  | N/A                    |
| JCD-10.1    | 4' x 6.5' x 3'     | 78 cu. ft.  | 5,441 lbs.  | \$6,509 (72 cu. ft.)   |
| No. 23      | 4.5' x 8.5' x 6.5' | 249 cu. ft. | 15,552 lbs. | \$19,337 (224 cu. ft.) |
| Attachment  |                    |             |             |                        |

| JCD-10.3 | 6' x 12' x 7' | 504 cu. ft. | 28,225 lbs. | \$15,331 (504 cu. ft.) |  |
|----------|---------------|-------------|-------------|------------------------|--|
|          |               |             |             |                        |  |

See Attachment No. 23

**INTERROGATORY NO. 24(a):** Referring to AT&T/WorldCom witness Donovan's supplemental rebuttal testimony filed February 11, 2002, page 10, lines 4-9, please explain how Exhibit JCD-10 shows the number of cables that can be accommodated by a given size manhole.

**<u>AT&T/MCI's Response</u>**: One indicator as to the number of cables that can be accommodated by each of the 4 manholes diagramed in Exhibit/Attachment JCD-10 is by observing the number of cable openings in each manhole. Exhibit JCD-10.1 has been annotated and attached to this response to show the number of large cables that could enter each of the sides of the manhole in Exhibit JCD-10.1. Manhole manufacturers will provide as many knock-outs (cable entrance holes), and in any format, as may be ordered by a telecommunications company. The particular configuration shown in Exhibit JCD-10.1 allows for cables to enter the manhole via four 4-inch holes in one end, two 4-inch holes in at least one side, plus any number of cables entering the manhole via the 12-inch by 28-inch slot in one end and the 6-inch by 28-inch slot in the side of the manhole. I demonstrate how at least 18 cables could enter such a manhole.

Exhibit JCD-10.2 has been annotated and attached to this response to show the number of large cables that could enter each of the sides of the manhole in Exhibit JCD-10.2. The particular configuration shown in Exhibit JCD-10.2 allows for cables to enter the manhole via four 4-inch cable entrance conduit holes in each of three sides of the manhole,

plus two 4-inch cable entrance conduit holes and a 6-inch by 28-inch slot in one side. I demonstrate how at least 18 cables could enter such a manhole.

Attachment JCD-10.3 shows a large 6-foot wide by 7-foot high by 12-foot long 504 cubic-foot manhole, with twelve 4-inch cable entrance conduit holes in each of the four sides of the manhole – in effect allowing for 48 cables being able to enter such a manhole.

Attachment JCD-10.4 shows a small 3-foot wide by 3-foot high by 3-foot long manhole, with nine 4-inch cable entrance conduit holes in one side and a 24-inch by 24-inch square hole in an adjacent side. It may be assumed that such a manhole would allow for at least 18 cables to enter such a manhole.

Another requirement for manhole capacity is the space required for cylindrical splice enclosures (called "splice cases"). I have included information (*AT&T Outside Plant Engineering Handbook, August 1994*, page 15-51) on splice case sizes as an attachment to this response that indicates splice case sizes vary from 2-inches in diameter by 21.5-inches long to 7-inches in diameter by 28.5-inches long, depending on the diameter of the cables being spliced. I have also included information as to how splice cases are frequently staggered in a manhole (*AT&T Outside Plant Engineering Handbook, August 1994*, pages 8-50 and 8-51).

See Attachment No. 24a.

<u>INTERROGATORY NO. 24(b)</u>: Referring to AT&T/WorldCom witness Donovan's supplemental rebuttal testimony filed February 11, 2002, page 10, lines 4-9, please identify the size and diameter of the cables assumed to be accommodated by the manholes shown in JCD-10.

AT&T/MCI's Response: Cables diameters can vary from 0.49 inch (for fiber cable and

small pair count copper cable) to 3.35 inches (for the largest 4200-pair 26-guage cable). I have attached information regarding such cable sizes to this response (*AT&T Outside Plant Engineering Handbook, August 1994*, pages 14-10, 14-19, 14-20, and 14-70).

See Attachments No. 24b.

**INTERROGATORY NO. 25:** Referring to AT&T/WorldCom witness Donovan's supplemental rebuttal testimony filed February 11, 2002, page 11, lines 6-11, please identify or otherwise demonstrate that BellSouth has double counted the costs described herein.

**<u>AT&T/MCI's Response</u>:** BellSouth's reply to *AT&T/WorldCom's 1st Set of Interrogatories, Item No. 5* provides descriptions of those items included in the Exempt Material category that BellSouth applied as part of its 40% factor. Appropriate pages of that response are included as an attachment to this response. BellSouth's Exempt Material costs include items such as the following:

Collar Manhole (BST Response pg. 28 of 71)

Cover Handhole (BST Response pg. 32 of 71)

Cover Manhole (BST Response pg. 32 of 71)

Cover Manhole with Locking Bolts (BST Response pg. 32 of 71)

Frame & Cover Manhole (BST Response pg. 36 of 71)

Frame Manhole (BST Response pg. 36 of 71)

Ring (Collar) Extension Manhole (BST Response pg. 55 of 71)

In addition, in response to AT&T and MCI's 3rd Set of Interrogatories, Item No. 35,

BellSouth admitted that,

Typically, manhole covers are provided by contractors and as such, the cost of the manhole covers is included in the total vendor installation costs. In those cases where Bellsouth provides the manhole covers, the cost of the manhole covers is classified to exempt material. Manhole covers, when furnished by BellSouth, meet the definition of exempt material being of small value, generally not reused when recovered from plant, and impractical to report on an individual basis when placed or recovered.

This BellSouth admission substantiates the double counting claim asserted by Mr. Donovan in BellSouth's 100% application of all Exempt Material loadings on top of Manhole Costs and even on top of Manhole Cover costs.

See Attachment No. 25.

**INTERROGATORY NO. 26:** Referring to AT&T/WorldCom witness Donovan's supplemental rebuttal testimony filed February 11, 2002, page 12, please identify the specific source of each of the values in the table at the top of the page.

**<u>AT&T/MCI's Response</u>**: The values in the boxes of the table from Mr. Donovan's supplemental rebuttal testimony, as shown above, have been labeled with code letters to assist in this explanation.

{a} Contract unit cost of \$16.90 may be observed in several places within BellSouth's submission, including in the table on page 25, near lines 21 & 22 of Ms. Caldwell's Surrebuttal Testimony as Amended January 28, 2002, as the cost per cubic foot for manholes greater than or equal to 351 cubic feet in size. Ms. Caldwell indicates that this "Per Cubic Foot [value is] based on M031B value in State Total sheet of the Contractor tables." This number was calculated by BellSouth as the total contractor cost for six 504 cu. ft. manholes divided by the total cubic feet for those six manholes (3024 cu. ft.). As discussed in Mr. Donovan's rebuttal testimony, this most cost effective number should be used to calculate manhole costs of any dimensions, not the more abhorrent number of \$48.06 cost per cubic foot as claimed by Ms. Caldwell for smaller manholes. {b} Same explanation as for {a}, however there is no disagreement as to the costper cubic foot for larger manholes.

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{c} BellSouth now agrees with Mr. Donovan regarding the appropriate cost of a manhole cover, as discussed in Ms. Caldwell's Surrebuttal Testimony as Amended January 28, 2002. On page 26, line 1 of that testimony, Ms. Caldwell states that, "Per Cover costs developed as the sum of total incurred cover costs divided by the number of covers using M045-M056 entries in the State Total sheet of the Contractor tables."

Other entries in the first table reflect AT&T/WorldCom's position, as supported by Mr. Donovan's expert opinion and testimony, that the loading factors applied by BellSouth are inappropriate for this category.

{d} Per Ms. Caldwell's Surrebuttal Testimony as Amended January 28, 2002, page 26 table, a manhole capable of housing 1 cable is 72 cubic feet in size  $(3' \times 4' \times 6' = 72)$ cu. ft.). AT&T agrees with this manhole size for one cable.

{e} Same explanation as for {d}, except that the capacity of the manhole is for one capable of housing 2 cables.

{f} Same explanation as for {d}, except that the capacity of the manhole is for one capable of housing 3 cables. AT&T/WorldCom's position, as supported by Mr. Donovan's expert opinion and testimony, indicate the reasons why a 3-foot by 4-foot by 6foot manhole of 72 cubic feet is perfectly capable of housing at least 3 or 4 cables. BellSouth disagrees, instead claiming that a very large 4-foot by 8-foot by 7-foot manhole of 224 cubic feet is required for only 3 cables.

7

{g} AT&T/WorldCom's position, as supported by Mr. Donovan's expert opinion and testimony, indicate the reasons why a 4-foot by 8-foot by 7-foot manhole of 224 cubic feet is more than adequate to handle 5 or more cables.

{h} AT&T/WorldCom's position, as supported by Mr. Donovan's expert opinion and testimony, is that BellSouth's alleged cost of \$16.90 per cubic foot without loadings, is the appropriate cost for all sizes of manholes.

 $\{i\}$  Same as  $\{h\}$ .

. '

- $\{j\}$  Same as  $\{h\}$ .
- $\{k\}$  Same as  $\{h\}$ .
- {1} Calculation of 72 cu. ft. {d} times 16.90/cu. ft. {h} = 1,216.88

{m} Calculation of 72 cu. ft. {e} times 16.90/cu. ft. {i} = 1,216.88

{n} Calculation of 72 cu. ft. {f} times 16.90/cu. ft. {j} = 1,216.88

{o} Calculation of 224 cu. ft. {g} times  $16.90/cu. ft. {k} = 3,785.60$ 

{p} Cost of one manhole cover, as agreed to by BellSouth, see explanation under{c} above, without loadings.

{q} Calculation of Manhole Cost 1,216.88 {l} plus Manhole Cover Cost 246.48 {p} = 1,463.36

{r} Calculation of Manhole Cost 1,216.88 {m} plus Manhole Cover Cost 246.48 {p} = 1,463.36

{s} Calculation of Manhole Cost 1,216.88 {n} plus Manhole Cover Cost 246.48 {p} = 1,463.36

{t} Calculation of Manhole Cost 3,785.60 {o} plus Manhole Cover Cost 246.48 {p} = 4,032.08

**INTERROGATORY NO. 27:** Referring to AT&T/WorldCom witness Donovan's supplemental rebuttal testimony filed February 11, 2002, page 15, lines 14-18, please identify all documents that support these statements.

<u>AT&T/MCI's Response</u>: Please see the response to request No. 25 which provides additional evidence as to BellSouth's admissions that contractor costs normally include all exempt materials, such as manhole covers.

In addition, and typical of all of the contractor costs used by BellSouth in this proceeding, BellSouth states in response to AT&T and MCI's 3rd Set of Interrogatories, Item No. 33:

M031A – Excavate and Place Pre-Cast Manhole that falls within the inside measurement of 151 cubic feet to 350 cubic feet. Manhole and associated hardware furnished and installed by contractor. Price per cubic foot.

M031B – Excavate and Place Pre-Cast Manhole that falls within the inside measurement of 351 cubic feet to 900 cubic feet. Manhole and associated hardware furnished and installed by contractor. Price per cubic foot.

BellSouth claims throughout its testimony that the contractor costs submitted in this proceeding are actual incurred costs placed on its investment books (whether efficient or not). Such costs are booked at full cost.

# INTERROGATORY NO. 28: For purposes of the following requests, please refer to AT&T/WorldCom witness Donovan's Exhibit JCD-9.

General Response:

All of source cost data is based on the data submitted by BellSouth in its revised cost filing and its responses to WorldCom's 1st Interrogatories Item No. 2, in which BellSouth states, "The Cost Data Below is Based on an RTAP [ARGUS] Extract Of 1997 [1998] [1999] [2000] Florida Cable & Wire Additions Data."

An Excel spreadsheet is being provided in response to this question which contains the costs provided by BellSouth on individual sheets by year in Tab 2 - *Data*, and accumulates those costs into Mr. Donovan's Exhibit JCD-9 in Tab 1 - *Factor*.

<u>INTERROGATORY NO. 28(a)</u>: Please identify the specific sources for each of the values in the columns labeled "Total 1997-2000, Labor" and "Total 1997-2000, Engineering."

**<u>AT&T/MCI's Response</u>**: The *Total 1997 – 2000 Labor* costs by Account are the sum of individual *Total Labor* costs provided by BellSouth for each of the four years (consisting of *Telco Labor* plus *Vendor Labor*).

The *Total 1997 – 2000 Engineering* costs by Account are the sum of individual *Total Engineering* costs provided by BellSouth for each of the four years (consisting of *Telco Engineering* plus *Vendor Engineering*).

**INTERROGATORY NO. 28(b):** Are the values in the columns referred to in (a) in dollars?

AT&T/MCI's Response: Yes.

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**INTERROGATORY NO. 28(c)**: If the response to (b) is affirmative, please explain how a ratio of the number of engineers to technicians supported can be derived from such data.

AT&T/MCI's Response: An estimate of the span of control of engineers to

10

technicians was derived based on the assumption that the cost per hour for an outside plant technician is approximately the same as for an engineer (BellSouth Worksheet 99Lab\_xls indicates Directly Assigned labor rates of \*\*\*BEGIN PROPRIETARY \$38.51/hr. END PROPRIETARY\*\*\* for Outside Plant Construction technicians and \*\*\*BEGIN PROPRIETARY \$39.52/hr END PROPRIETARY\*\*\* for Outside Plant Engineers). Based on labor rate date in BellSouth as well as in other ILECs, this appears to be a reasonable assumption supported by our expert outside plant witness, Mr. Donovan.

**INTERROGATORY NO. 28(d)**: Please identify the specific sources for each of the values in the column labeled "TELRIC Engineering Cost."

**AT&T/MCI's Response:** The *TELRIC Engineering Cost* is based on the presumption that one engineer should be able to keep 6 outside plant technicians busy, as supported by Mr. Donovan's rebuttal testimony. Therefore the *TELRIC Engineering Cost* shown in Exhibit JCD-9 is the product of the *Total 1997 – 2000 Labor* cost by *Account* times the *TELRIC Ratio of Engineering to Labor* @ 1:6 of 16.7%.

**INTERROGATORY NO. 28(e)**: Please identify the specific sources for each of the values in the column labeled "Total Less Engineering."

**AT&T/MCI's Response:** The *Total Less Engineering* cost is the summation of BellSouth's submitted *Telco Labor + Vendor Labor + Exempt Material + Non-Exempt Material + Other* for years 1997 through 2000.

See Attachment No. 28e.

**INTERROGATORY NO. 29:** For the following questions, please refer to Exhibit BFP-18, pages one through six, and to the column on the far right of each page labeled

"AT&T-WCom Input."



**INTERROGATORY NO. 29(a):** Please identify the location in the witness' testimony, either in rebuttal, deposition, or supplemental rebuttal, where evidence or support is offered for each specific input.

AT&T/MCI's Response: See Attachment No. 29.

**INTERROGATORY NO. 29(b):** Please identify the page and line number in the witness' testimony, either in rebuttal, deposition, or supplemental rebuttal, where evidence or support is offered for each specific input.

AT&T/MCI's Response: See Attachment No. 29.

DATED this 4th day of March, 2002

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| Acct | Asset _                | Total 1993<br>Labor | 7 - 2000<br>Engineering | of Engi | led Ratio<br>ineering<br>.abor | TELRIC Ratio<br>of Engineering<br>to Labor @ 1:6 | TELRIC<br>Engineering<br>Cost | Total Less<br>Engineering | TELRIC BSTLM<br>Engineering<br>Factor Input |
|------|------------------------|---------------------|-------------------------|---------|--------------------------------|--|-------------------------------|---------------------------|---|
| 822C | Aerial Fiber           | 9,274.574           | 1,795,914               | 19.4%   | = 1 : 5.2                      | <u>16.7%</u>                                     | <u>1.545.762</u>              | 23,393,488                | 7%  |
| 5C   | Underground Copper     | 17,256,750          | 3,679,257               | 21.3%   | = 1 : 4.7                      | 16.7%  | 2,876,125                     | 38,794,345                | 7%  |
| 845C | Buried Fiber           | 97,805,056          | 24,879,493              | 25.4%   | = 1 : 3.9                      | 16.7%  | 16,300,843                    | 146,912,560               | 11%   |
| 4C   | Conduit                | 26,011,264          | 6,802,758               | 26.2%   | = 1 : 3.8                      | 16.7%  | 4,335,211                     | 36,205,300                | 12%   |
| 85C  | Underground Fiber      | 16,635,134          | 5,003,841               | 30.1%   | = 1 : 3.3                      | 16.7%  | 2,772,522                     | 60,019,443                | 5%  |
| 852C | Intrabuilding Fiber    | 256,303             | 77,751                  | 30.3%   | = 1 : 3.3                      | 16.7%  | 42,717                        | 465,166                   | 9%  |
| 22C  | Aerial Copper          | 28,991,677          | 9,258,892               | 31.9%   | = 1 : 3.1                      | 16.7%  | 4,831,946                     | 66,220,452                | 7%  |
| 45C  | Buried Copper          | 183,321,710         | 59,476,324              | 32.4%   | = 1 : 3.1                      | 16.7%  | 30,553,618                    | 298,342,992               | 10%   |
| 812C | Aerial Fiber Entrance  | 3,412,076           | 1,535,331               | 45.0%   | = 1 : 2.2                      | 16.7%  | 568,679                       | 6,546,037                 | 9%  |
| 52C  | Intrabuilding Copper   | 1,626,613           | 954,038                 | 58.7%   | = 1 : 1.7                      | 16.7%  | 271,102                       | 3,450,039                 | 8%  |
| 1C   | Poles                  | 6,304,347           | 3,717,327               | 59.0%   | = 1 : 1.7                      | 16.7%  | 1,050,725                     | 11,166,845                | 9%  |
| 12C  | Aerial Copper Entrance | 13,629,261          | 12,763,258              | 93.6%   | = 1 : 1.1                      | 16.7%  | 2,271,543                     | 26,649,400                | 9%  |
|      | Total                  | 404,524,764         | 129,944,184             | 32.1%   | = 1 : 3.1                      | 16.7%  | 67,420,794                    | 718,166,066               | 9.4%  |

#### ENGINEERING FACTOR DEVELOPMENT

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|   | ENGINEERING FACTOR DEVELOPMENT                           |  |  |  |  |   |  |   |  |  |                            |  |  |   |  |  |  |  |
|---|--|--|--|--|--|---|--|---|--|--|----------------------------|--|--|---|--|--|--|--|
|   |  | Telco<br>Labor   | Vendor<br>Labor  | Total<br>Labor   | E                                      | Telco<br>ngineering   | E  | Vendor<br>ngineering  | E  | Total<br>Engineering   |                            | Exempt<br>Material   | N  | on-Exempt<br>Material   |  | Total<br>Material  |  | Other Total  |
| which a share of the second   | a Belo   | ow is Based  | On An RTAP Ex  | tract Of 1997 F  | lorid                                  | a Cable & Wir   | e A  | ditions Data  |  |  |                            |  |  |   |  |  |  |  |
| 1C<br>5C<br>12C<br>22C<br>45C<br>52C<br>85C   | \$<br>\$   | 286,372<br>4,301,849   | \$ 212,690<br>\$ 232,370<br>\$ 29,018,923<br>\$ 3,382<br>\$ 163,129  | \$289,754<br>\$4,464,978   | \$<br>\$<br>\$<br>\$<br>\$<br>\$       | 518,819<br>1,095,629<br>1,039,396<br>4,650,260<br>62,849<br>792,321   | \$<br>\$<br>\$<br>\$<br>\$   | 746,581<br>941,346<br>6,474,657<br>17,292<br>604,435  | \$ \$ \$ \$ \$ \$                            | 1,014,742<br>1,842,210<br>1,980,742<br>11,124,917<br>80,141<br>1,396,756   | \$<br>\$<br>\$<br>\$<br>\$ | 1,886,928<br>1,275,812<br>2,724,139<br>6,307,354<br>136,364<br>1,920,668   | \$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$ | 1,916,026<br>7,610,252<br>26,510,871<br>701,679<br>11,605,764   | \$<br>\$<br>\$                                 | 3,191,838<br>10,334,391<br>32,818,225<br>838,043<br>13,526,432   | \$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$ | 201,245         \$ 12,627,831           (307,265)         \$ 7,482,495           2,940,394         \$ 20,967,009           4,182,733         \$ 89,765,097           (108,672)         \$ 10,99,266           (327,192)         \$ 19,060,974  |
| 812C<br>822C<br>845C<br>852C<br>4C<br>Total   | \$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$       | 1,083,164<br>3,986,500<br>19,052   | \$ 34,316<br>\$ 63,210<br>\$ 8,781,871<br>\$ -<br>\$ 38,801,512  | \$ 19,052  |  | 150,772<br>135,144<br>892,320<br>31,080<br>9,368,590  |  | 130,693<br>138,616<br>1,457,293<br>1,302<br>11,008,138  | \$ \$ \$ \$ \$<br>\$                         | 281,465<br>273,760<br>2,349,613<br>32,382<br>20 376 728  | \$                         | 355,941<br>535,478<br>1,890,224<br>8,580<br>17,041,488   | \$<br>\$<br>\$<br>\$<br>\$<br>\$                         | 264,688<br>1,797,614<br>6,934,890<br>8,903<br>62,643,564  | \$<br>\$                                       | 8,825,114<br>17,483  | \$   | (7,602) \$ 1,678,309<br>52,760 \$ 3,805,986<br>172,951 \$ 24,116,049<br>(3,874) \$ 65,043<br>6,795,478 \$180,668,059   |
|   |  |  | On An RTAP E   | . , ,  |  |   |  |   | φ  | 20,370,728   | 4                          | 17,041,400   | ¢  | 02,043,304  | Φ  | 79,005,052   | ą  | 0,790,478 \$ 100,000,009   |
| 1C<br>5C<br>12C<br>22C<br>45C<br>52C<br>85C<br>812C<br>845C<br>852C<br>852C<br>4C                           | * * * * * * * * * * * *                                  | 596,247<br>4,758,156<br>3,261,944<br>5,552,209<br>12,763,450<br>412,308<br>4,045,140<br>754,784<br>1,389,227<br>3,583,749<br>41,912<br>1,375,177   | \$ 1,452,456<br>\$ 395,760<br>\$ 124,830<br>\$ 145,572<br>\$ 31,672,858<br>\$ 16,093<br>\$ 243,189<br>\$ 61,908<br>\$ 24,595<br>\$ 11,123,809<br>\$ -<br>\$ 9,446,104  | \$ 2,048,703<br>\$ 5,153,916<br>\$ 3,386,774<br>\$ 5,697,781<br>\$ 44,436,308<br>\$ 428,401<br>\$ 4,288,329<br>\$ 816,692<br>\$ 1,413,822<br>\$ 14,707,558<br>\$ 41,912<br>\$ 10,821,281   | * * * * * * * * * * *                  | 18,479<br>94,999<br>1,195,943<br>177,125<br>514,496<br>222,207<br>307,965<br>179,621<br>21,842<br>128,877<br>2,074<br>2,822   | \$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$<br>\$ | 1,528,112<br>800,443<br>2,145,277<br>1,506,736<br>13,966,096<br>55,392<br>1,100,646<br>200,878<br>336,085<br>5,924,130<br>4,993<br>2,601,129  | * * * * * * * * * * *                        | 1,546,591<br>895,442<br>3,341,220<br>1,683,861<br>14,482,592<br>277,599<br>1,408,611<br>380,499<br>357,927<br>6,053,007<br>7,067<br>2,603,951  | \$<br>\$                   | 318,567<br>2,462,924<br>1,700,011<br>2,892,888<br>6,477,403<br>220,892<br>1,846,926<br>407,331<br>654,041<br>1,611,419<br>22,710<br>737,025  | * * * * * * * * * * *                                    | 10,886,110<br>299,366<br>2,267,078<br>9,335,247   | \$   | $\begin{array}{c} 1,823,188\\ 5,102,738\\ 3,316,647\\ 5,421,804\\ 19,517,564\\ 364,255\\ 12,733,036\\ 706,697\\ 2,921,119\\ 10,946,666\\ 32,979\\ 2,331,794 \end{array}$                   | ****   | (181,145) \$ 5,237,337<br>(93,820) \$ 11,058,276<br>(367,690) \$ 9,676,951<br>2,332,672 \$ 15,136,118<br>5,819,095 \$ 84,255,559<br>(54,401) \$ 1,015,854<br>316,032 \$ 18,746,008<br>(11,510) \$ 1,892,378<br>145,271 \$ 4,838,139<br>773,193 \$ 32,480,424<br>- \$ 81,958<br>195,220 \$ 15,952,246   |
| Total   | \$   | 38,534,303   | \$ 54,707,174  | \$ 93,241,477  | \$                                     | 2,866,450   | \$   | 30,171,917  | \$   | 33,038,367   | \$                         | 19,352,137   | \$   | 45,866,350  | \$   | 65,218,487   | \$   | 8,872,917 \$200,371,248  |
| 1C<br>5C<br>12C<br>22C<br>45C<br>85C<br>812C<br>845C<br>845C<br>845C<br>852C<br>4C<br>Total                 | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 730,336<br>3,597,831<br>3,542,205<br>12,382,345<br>23,783,586<br>416,906<br>3,343,668<br>886,548<br>4,158,029<br>6,125,835<br>67,897<br>1,102,711<br>60,137,897<br>1,102,711<br>60,137,897<br>5,61,986<br>3,574,479<br>3,596,650<br>5,511,166<br>12,151,906<br>483,798<br>3,949,303<br>847,283<br>2,406,245<br>5,070,595<br>126,211<br>1,555,929 | On An RTAP Ex           \$ 1,559,832           \$ 395,728           \$ 166,969           \$ 121,783           \$ 34,285,353           \$ 4,285,353           \$ 4,285,353           \$ 4,285,353           \$ 34,285,353           \$ 34,285,353           \$ 34,285,353           \$ 30,053,749           \$ 55,347           \$ 30,053,749           \$ 7,158,274           \$ 74,098,161           OOD Florida Cabb           \$ 1,403,490           \$ 302,757           \$ 10,403,490           \$ 27,025,335           \$ 34,295           \$ 27,025,335           \$ 329,358           \$ 40,430           \$ 94,757           \$ 29,078,949           \$ 29,078,949           \$ 5,373,069           \$ 63,900,876 | \$ 2,290,168<br>\$ 3,993,559<br>\$ 3,709,174<br>\$ 12,504,128<br>\$ 58,068,939<br>\$ 421,231<br>\$ 3,603,165<br>\$ 923,853<br>\$ 4,213,376<br>\$ 36,179,584<br>\$ 4,213,376<br>\$ 36,179,584<br>\$ 4,213,376<br>\$ 36,79,584<br>\$ 4,260,599<br><b>Let &amp; Wire Additi</b><br>\$ 1,965,476<br>\$ 3,3777,236<br>\$ 3,3777,236<br>\$ 3,3777,237<br>\$ 4,278,662<br>\$ 39,177,241<br>\$ 487,227<br>\$ 4,278,662<br>\$ 38,71741<br>\$ 487,227<br>\$ 4,278,662<br>\$ 38,71741<br>\$ 487,227<br>\$ 4,278,662<br>\$ 38,7142<br>\$ 2,501,002<br>\$ 34,149,543<br>\$ 2,501,002<br>\$ 34,149,543<br>\$ 2,501,002<br>\$ 34,149,543<br>\$ 2,501,002<br>\$ 34,149,543<br>\$ 2,501,002<br>\$ 34,149,543<br>\$ 2,501,002<br>\$ 34,149,543<br>\$ 2,501,002<br>\$ 38,7141<br>\$ 2,501,002<br>\$ 38,7142<br>\$ 3,502,502<br>\$ 38,7142<br>\$ 3 | ************************************** | 492,777<br>349,093<br>2,226,136<br>6,197,264<br>287,693<br>343,666<br>289,942<br>482,989<br>3,913,644<br>7,434<br>831,844<br>16,733,121   | *  | dditions Data<br>784,907<br>463,139<br>1,545,608<br>1,060,527<br>8,361,749<br>69,437<br>858,213<br>159,194<br>501,086<br>4,741,532<br>9,816<br>4,741,532<br>9,816<br>4,741,535<br>19,746,595<br>305,067<br>260,724<br>1,025,346<br>780,465<br>8,674,133<br>4,199<br>612,090<br>48,151<br>57,285<br>3,869,875<br>3,869,875 | *****  | $\begin{array}{c} 1,277,684\\ 812,232\\ 3,771,744\\ 2,371,166\\ 14,559,013\\ 357,130\\ 1,201,879\\ 449,136\\ 8,655,176\\ 17,250\\ 2,023,231\\ 36,479,717\\ 893,052\\ 956,841\\ 3,808,084\\ 3,223,123\\ 19,309,802\\ 239,168\\ 996,595\\ 424,231\\ 180,151\\ 180,151\\ 7,821,697\\ 21,052\\ 2,175,576\\ 40,049,372\\ \end{array}$ | ********                   | 218,317<br>1,516,961<br>500,938<br>2,094,286<br>3,619,947<br>32,465<br>617,563<br>35,142,912<br>344,332<br>3,198,040<br>2,078,733<br>4,863,560<br>15,221,512<br>2,77,157<br>2,050,199<br>489,399<br>1,640,350<br>2,975,719<br>82,049 |  | 15,552<br>3,354,753<br>41,445,429<br>1,450,359<br>1,978,680<br>1,822,865<br>2,111,174<br>10,368,745<br>209,860<br>7,111,580<br>499,975<br>1,846,586<br>8,865,170<br>34,189<br>2,552,541 | ************                                   | 48,016<br>3,972,316<br>76,588,338<br>1,794,691<br>5,176,720<br>3,901,598<br>6,974,734<br>25,590,256<br>487,017<br>9,161,779<br>9,79,373<br>3,486,936<br>11,840,889<br>116,238<br>3,454,566 | * * * * * * * * * * * * * * * * * * *                                |  |
| Aggregate for<br>1C<br>5C<br>12C<br>22C<br>45C<br>52C<br>85C<br>812C<br>845C<br>845C<br>852C<br>4C<br>Total | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$                      | 1,888,569<br>15,870,884<br>12,943,821<br>28,424,832<br>61,319,241<br>1,599,384<br>15,639,960<br>3,238,116<br>9,036,665<br>18,766,679<br>255,072<br>4,033,817   | \$ 4,415,778<br>\$ 1,385,866<br>\$ 685,440<br>\$ 566,845<br>\$ 122,002,469<br>\$ 27,228<br>\$ 995,173<br>\$ 173,959<br>\$ 237,909<br>\$ 79,038,378   | <ul> <li>\$ 1,626,613</li> <li>\$ 16,635,134</li> <li>\$ 3,412,076</li> <li>\$ 9,274,574</li> <li>\$ 97,805,056</li> <li>\$ 256,303</li> <li>\$ 26,011,264</li> </ul>  | * * * * * * * * * * *                  | $\begin{array}{c} 1,099,241\\ 1,659,028\\ 7,300,446\\ 4,969,818\\ 21,997,689\\ 807,719\\ 1,828,457\\ 996,415\\ 762,841\\ 8,886,664\\ 61,640\\ 2,058,883\\ 52,428,840\\ \end{array}$ | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$  | 146,320<br>3,175,384<br>538,916<br>1,033,072<br>15,992,830<br>16,111<br>4,743,875<br>77,515,343   | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 3,679,257<br>12,763,258<br>9,258,892<br>59,476,324<br>954,038<br>5,003,841<br>1,535,331<br>1,795,914<br>24,879,493<br>77,751<br>6,802,758  | * * * * * * * * * * * * *  | 7,038,962<br>17,546,362<br>43,015,080<br>852,730<br>7,334,754<br>1,753,609<br>4,924,155<br>10,097,309<br>145,804<br>2,256,613<br>105,659,611   | * * * * * * * * * *                                      | 12,134,628<br>7,289,900<br>14,626,960<br>58,672,898<br>1,191,737<br>36,420,770<br>1,445,907<br>8,570,867<br>36,441,602<br>68,913<br>7,502,063   | \$ \$ \$ \$ \$ \$ \$ \$ <b>\$</b> \$ <b>\$</b> | 32,173,321<br>101,687,977<br>2,044,466<br>43,755,524<br>3,199,515<br>13,495,021<br>46,538,911<br>214,716<br>9,758,676  | * * * * * * * * * *  | (640,979)         \$ 14,884,172           (218,612)         \$ 42,473,602           (1,308,724)         \$ 39,412,658           5,055,453         \$ 75,479,343           13,333,305         \$ 357,819,316           (221,040)         \$ 4,404,077           (371,214)         \$ 65,023,284           (65,554)         \$ 8,081,368           623,893         \$ 25,189,402           2,566,592         \$ 171,792,053           (5,854)         \$ 542,917           435,360         \$ 43,008,058           19,184,626         \$ 848,110,250 |

DECLASSIFIED

CONTAINS BELLSOUTH PROPRIETARY INFORMATION

# BEFORE THE FLORIDA PUBLIC SERVICE COMMISSION

In re: Investigation into pricing of unbundled network elements Docket No. 990649A-TP

## AT&T COMMUNICATIONS OF THE SOUTHERN STATES, INC. AND MCI WORLDCOM, INC.'S JOINT RESPONSES TO FPSC STAFF'S THIRD REQUEST FOR PRODUCTION OF DOCUMENTS

AT&T Communications of the Southern States, Inc. ("AT&T") and MCI WorldCom, Inc. ("MCI"), pursuant to Rule 28-106.206, Florida Administrative Code and Rules 1.350 and 1.280, Florida Rules of Civil Procedure, hereby submit the following Responses to FPSC Staff's Third Request for Production of Documents to AT&T and MCI.

### **DOCUMENT REQUESTS:**

<u>REQUEST NO. 23</u>: Please provide all documents identified in response to Interrogatory No. 22.

**<u>AT&T/MCI's Response</u>**: The response to Interrogatory No. 22 indicates that the relevant passage of Mr. Donovan's testimony, the 1 engineer to 6 outside plant technicians "span of control" is based on Mr. Donovan's 30+ years of telecommunications experience, not on published documents.

REQUEST NO. 24:Please provide all documents identified in response toInterrogatory No. 23.CONDECCEPTIONS INFEDAT&T/MCI's Response:The response to Interrogatory No. 23 indicates that Mr.Donovan's testimony does not state that a smaller manhole could not ever cost more than a

larger manhole – just that such a pricing structure is illogical, based on his 30+ years of hands-on telecommunications experience. His opinion is not based on published documents,

This claim of confidentiality was filed by or on behalf of a "telco" for Confidential DN <u>02487-02</u>. The document is in locked storage pending advice on handling. To access the material, your name must be on the CASR. If undocketed, your division director must obtain written EXD/Tech permission before you can access it.

02487 HAR-48

DOCUMENT NUMBE

FPSC-COMMISSION CLERK,

Appropriate documents support the response are attached to that response, or have been supplied in testimony.

<u>REQUEST NO. 25</u>: Please provide all documents identified in response to Interrogatory No. 24(b).

**<u>AT&T/MCI's Response</u>**: A copy of the *AT&T Outside Plant Engineering Handbook, August 1994*, pages 14-10, 14-19, 14-20, and 14-70 have been provided as an attachment to Interrogatory No. 24(b).

<u>REQUEST NO. 26</u>: Please provide all documents identified in response to Interrogatory No. 25.

<u>AT&T/MCI's Response</u>: Appropriate pages from BellSouth's reply to *AT&T/WorldCom's 1st Set of Interrogatories, Item No. 5*, have been provided as an attachment to Interrogatory No. 25.

<u>REQUEST NO. 27</u>: Please provide all documents identified in response to Interrogatory No. 27.

**<u>AT&T/MCI's Response</u>**: All calculations are described in the response to Interrogatory No. 27. The only documents required in support of those calculations were provided in testimony and are specifically identified for each appropriate cell in the table. There are no additional documents.

<u>REQUEST NO. 28</u>: Referring to AT&T/WorldCom witness Donovan's Exhibit JCD-9:

**<u>REQUEST NO. 28(a)</u>**: Please provide any and all work papers that support this exhibit, including any underlying spreadsheet files.

2

**<u>AT&T/MCI's Response</u>**: Work papers consist of the Excel spreadsheets that were provided in response to Interrogatory No. 27. There are no additional documents.

**<u>REQUEST NO. 28(b)</u>**: To the extent not self-evident in the work papers provided in response to (a), please indicate the specific calculations performed.

**<u>AT&T/MCI's Response</u>**: AT&T/WorldCom believes that the information provided in response to Interrogatory No. 28 provides adequate information to indicate the specific calculations performed. Those calculations simply sum the four years of data provided by BellSouth for 1997 through 2000, and provide straightforward arithmetic calculations. Mr. Donovan can be reached on 516-739-3565 if there are any questions about a calculation.

**REQUEST NO. 28(c)**: Please provide all documents identified in response to Interrogatory No. 28. To the extent that any such documents have been previously provided in this proceeding, please identify in which request it was provided.

**<u>AT&T/MCI's Response</u>**: The response to Interrogatory No. 28 references an Excel Workbook file provided as an attachment to that response. In addition, the assumption that a span of control for engineers to construction technicians can be derived via a ratio of engineering dollars to construction direct labor dollars, because the labor rates are nearly identical refers to Directly Assigned labor rates provided by BellSouth in this proceeding as Worksheet 99Lab\_xls, as indicated in the response to Interrogatory No. 28.

<u>REQUEST NO. 29</u>: BFP-15 attached to witness Pitkin's February 11, 2002, Supplemental Rebuttal Testimony, page 3 of 12, shows a comparison of BellSouth's Forecast of Telephone Plant Indexes as filed by BellSouth, updated for 1998-2001 actuals and new BellSouth projections, and updated for material-only actuals 1998-2001 and new BellSouth projections. The source for the 1998-2001 actuals is noted as

3

RL:01-11-005BT, Attachment 3, pages 1 and 2, BellSouth's "November 2001 Forecast of % Cost Change." This attachment indicates 2000, actual percent change but not 2001. Provide the source document for the 2001, actuals shown in BFP-15.

**AT&T/MCI's Response:** The 2001 actuals for material and labor combined shown in Attachment BFP-15 are located in BellSouth's response to AT&T / WorldCom Item 36 Attachment 2 pages 2-3. For material only, the actuals shown in Attachment BFP-15 are located in BellSouth's response to AT&T / WorldCom Item 36 Attachment 2 pages 4-6. (The relevant pages from this discovery response are included as pages 4-12 of BFP Attachment 15.) The note "RL:01-11-005BT, Attachment 3, pages 1 and 2" refers to BellSouth's projections.

<u>REQUEST NO. 30</u>: For each AT&T/WorldCom updated input shown on BFP-18, provide all workpapers, LOTUS spreadsheets, and calculations showing the step-bystep development of each input.

AT&T/MCI's Response: See file included in response to Staff Interrogatory No. 29 ("Attachment to Interrogatory No. 29.xls").

DATED this 4<sup>th</sup> day of March, 2002

TRACY W. HATCH, ESQ. FLOYD R. SELF, ESQ. MESSER, CAPARELLO & SELF, P. A. Post Office Box 1876 Tallahassee, FL 32302-1876 (850) 222-0720

Attorney for AT&T Communications of the Southern States, Inc.

and

Donna McNulty, Esq. MCI WorldCom, Inc. The Atrium Building, Suite 105 325 John Knox Road Tallahassee, FL 32303 o

|                         |      | BellSouth |         | Actuals<br>With New | Material<br>With New |
|-------------------------|------|-----------|---------|---------------------|----------------------|
|                         |      | As Filed  | Actuals | BS Proj             | BS Proj              |
| Poles                   | 1C   | 7.68      | 3.06    | 2.63                | (3.84)               |
| Aerial Ca - Metal       | 22C  | 8.22      | 2.14    | 0.79                | (3.75)               |
| Buried Ca - Metal       | 45C  | 7.15      | 3.49    | 2.80                | 0.98                 |
| Conduit Systems         | 4C   | 7.00      | 5.50    | 4.72                | 6.93                 |
| Intrbld Network - Metal | 52C  | 9.26      | 1.43    | 0.09                | (4.85)               |
| Underground Ca - Metal  | 5C   | 9.26      | 2.28    | 0.60                | (2.65)               |
| Aerial Ca - Fiber       | 822C | 2.01      | 0.58    | 0.58                | (2.11)               |
| Buried Ca - Fiber       | 845C | 4.05      | 1.87    | 1.87                | (2.11)               |
| Introld Network - Fiber | 852C | 4.05      | 1.44    | 1.44                | (2.11)               |
| Underground Ca - Fiber  | 85C  | -         | (0.43)  | (0.43)              | (2.11)               |
| Digital Sub Pair Gain   | 257C | (2.00)    | (5.64)  | (6.26)              | N/A                  |
| Digital Electronics     | 377C | 2.01      | 2.02    | 1.68                | N/A                  |

#### CORRECTION OF BELLSOUTH'S INFLATION FORECASTS AND USE OF MATERIAL - ONLY INFLATION FACTORS

|                         |      | BellSouth<br>As Filed | Actuals | Actuals<br>With New<br>BS Proj | Material<br>With New<br>BS Proj |
|-------------------------|------|-----------------------|---------|--------------------------------|---------------------------------|
| Poles                   | 1C   | 7.68                  | (4.62)  | (5.05)                         | (11.52)                         |
| Aerial Ca - Metal       | 22C  | 8.22                  | (6.08)  | (7.43)                         | (11.96)                         |
| Buried Ca - Metal       | 45C  | 7.15                  | (3.66)  | (4.35)                         | (6.17)                          |
| Conduit Systems         | 4C   | 7.00                  | (1.50)  | (2.28)                         | (0.07)                          |
| Introld Network - Metal | 52C  | 9.26                  | (7.83)  | (9.17)                         | (14.11)                         |
| Underground Ca - Metal  | 5C   | 9.26                  | (6.97)  | (8.66)                         | (11.91)                         |
| Aerial Ca - Fiber       | 822C | 2.01                  | (1.44)  | (1.44)                         | (4.13)                          |
| Buried Ca - Fiber       | 845C | 4.05                  | (2.18)  | (2.18)                         | (6.17)                          |
| Introld Network - Fiber | 852C | 4.05                  | (2.62)  | (2.62)                         | (6.17)                          |
| Underground Ca - Fiber  | 85C  | -                     | (0.43)  | (0.43)                         | (2.11)                          |
| Digital Sub Pair Gain   | 257C | (2.00)                | (3.64)  | (4.26)                         | N/A                             |
| Digital Electronics     | 377C | 2.01                  | 0.00    | (0.34)                         | N/A                             |

Investment

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#### BellSouth Account Average Levelized Inflation Loadings For Forward Looking Studies 2000-2002, 1999 Vintage

| FRC  | 2000<br>A  | 2001   | 2002  |   |  |  |  | Inflation   |
|--|--|--|---|---|--|--|--|---|
|  | Α  | -  | 200Z  | 2000  | 2001   | 2002   | Total  | Loadings  |
|  |  | в  | С   | D   | E  | F  | G  | н   |
| 10   |  |  |   | =(1+(A/100))  | =(1+(B/100))*D   | =(1+(C/100))*E   | D+E+F  | =G/3  |
| 10   |  |  |   |   |  |  |  |   |
|  | 3.7  | 3.8  | 3.8   | 1.037340  | 1.076310   | 1,116846   | 3.230496   | 1.076832  |
| 22C  | 4.0  | 4.0  | 4.0   | 1.040000  | 1.081600   | 1,124864   |  | 1.082155  |
| 45C  | 4.0  | 3.0  | 3.0   | 1.040000  | 1.071200   | 1.103336   | 3.214536   | 1.071512  |
| 4C   | 3.2  | 3.7  | 3.5   | 1.032193  | 1.069996   |  | 3.209964   | 1.069988  |
| 52C  | 5.0  | 4.0  | 4.0   | 1.050000  | 1.092000   |  |  | 1.092560  |
| 5C   | 5.0  | 4.0  | 4.0   | 1.050000  | 1.092000   | 1.135680   | 3.277680   | 1.092560  |
| 822C   | 1.0  | 1.0  | 1.0   | 1.010000  | 1.020100   | 1.030301   | 3.060401   | 1.020134  |
| 845C   | 2.0  | 2.0  | 2.0   | 1.020000  | 1.040400   | 1.061208   | 3.121608   | 1.040536  |
| 852C   | 2.0  | 2.0  | 2.0   | 1.020000  | 1.040400   | 1.061208   | 3.121608   | 1.040536  |
| 85C  | 0.0  | 0.0  | 0.0   | 1.000000  | 1.000000   | 1.000000   | 3.000000   | 1.000000  |
| 257C   | -2.0   | 0.0  | 0.0   | 0.980000  | 0.980000   | 0.980000   | 2.940000   | 0.980000  |
| 377C   | 1.0  | 1.0  | 1.0   | 1.010000  | 1.020100   | 1.030301   | 3.060401   | 1.020134  |
| <u>s</u>   |  |  |   |   |  |  |  |   |
| 1C   | 0.8  | 1.5  | 3.8   | 1.008047  | 1.022677   | 1.061193   | 3.091917   | 1.030639  |
| 22C  | -0.1   | 1.3  | 4.0   | 0.999127  | 1.012227   |  |  | 1.021357  |
| 45C  | 1.5  |  | 3.0   |   |  |  |  | 1.034898  |
| 4C   | 2.9  | 2.0  | 3.5   |   | 1.049395   |  |  | 1.055025  |
| 52C  | -0.6   | 1.1  | 4.0   | 0.993648  | 1.004537   |  |  | 1.014301  |
| 5C   | 0.3  | 1.0  | 4.0   | 1.002710  | 1.012647   | 1.053153   | 3.068509   | 1.022836  |
| 822C   | -0.4   | 1.0  | 1.0   | 0.995646  | 1.005806   | 1.015864   | 3.017315   | 1.005772  |
| 845C   | 0.3  | 1.3  | 2.0   | 1.003476  | 1.016222   | 1.036547   | 3.056246   | 1.018749  |
| 852C   | -0.1   | 1.3  | 2.0   | 0.998658  | 1.012081   | 1.032322   | 3.043060   | 1.014353  |
| 85C  | -1.0   | 0.8  | 0.0   | 0.990323  | 0.998387   | 0.998387   | 2.987097   | 0.995699  |
| 257C   | -4.0   | -2.5   | 0.0   | 0.959854  | 0.935523   | 0.935523   | 2.830900   | 0.943633  |
| 377C   | -0.2   | 2.8  | 1.0   | 0.997990  | 1.026131   | 1.036392   | 3.060513   | 1.020171  |
| s and N  | ew Be  | ISout  | <u>n Proj</u> e   | ections   |  |  |  |   |
| 1C   | 0.8  | 1.5  | 2.5   | 1.008047  | 1.022677   | 1.048244   | 3.078969   | 1.026323  |
| 22C  | -0.1   | 1.3  | 0.0   | 0.999127  | 1.012227   |  |  | 1.007860  |
| 45C  | 1.5  | 1.4  | 1.0   | 1.015451  | 1.029185   | 1.039476   | 3.084112   | 1.028037  |
| 4C   | 2.9  | 2.0  | 1.3   | 1.029234  | 1.049395   | 1.063037   | 3.141666   | 1.047222  |
| 40   | -0.6   | 1.1  | 0.0   | 0.993648  | 1.004537   |  |  |   |
| 4C<br>52C  |  |  |   |   |  | 1.004537   | 3.002722   |   |
|  | 0.3  | 1.0  | -1.0  | 1.002710  | 1.012647   | 1.004537<br>1.002520   |  | 1.000907  |
| 52C  |  | 1.0<br>1.0   | -1.0<br>1.0   |   |  | 1.002520   |  | 1.000907<br>1.005959  |
| 52C<br>5C  | 0.3  |  |   | 1.002710  | 1.012647   | 1.002520   | 3.017877<br>3.017315   | 1.000907<br>1.005959<br>1.005772  |
| 52C<br>5C<br>822C  | 0.3<br>-0.4  | 1.0  | 1.0   | 1.002710<br>0.995646  | 1.012647<br>1.005806   | 1.002520<br>1.015864   | 3.017877<br>3.017315<br>3.056246   | 1.000907<br>1.005959<br>1.005772<br>1.018749  |
| 52C<br>5C<br>822C<br>845C  | 0.3<br>-0.4<br>0.3   | 1.0<br>1.3   | 1.0<br>2.0  | 1.002710<br>0.995646<br>1.003476  | 1.012647<br>1.005806<br>1.016222   | 1.002520<br>1.015864<br>1.036547   | 3.017877<br>3.017315<br>3.056246<br>3.043060   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353  |
| 52C<br>5C<br>822C<br>845C<br>852C  | 0.3<br>-0.4<br>0.3<br>-0.1   | 1.0<br>1.3<br>1.3  | 1.0<br>2.0<br>2.0   | 1.002710<br>0.995646<br>1.003476<br>0.998658  | 1.012647<br>1.005806<br>1.016222<br>1.012081   | 1.002520<br>1.015864<br>1.036547<br>1.032322   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>852C  | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0   | 1.0<br>1.3<br>1.3<br>0.8   | 1.0<br>2.0<br>2.0<br>0.0  | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323  | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387   | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397<br>1.016750  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>85C<br>257C<br>377C   | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-4.0<br>-0.2   | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8  | 1.0<br>2.0<br>2.0<br>0.0<br>-2.0<br>0.0   | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854  | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387<br>0.935523<br>1.026131   | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>85C<br>257C<br>377C   | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-4.0<br>-0.2   | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8  | 1.0<br>2.0<br>2.0<br>0.0<br>-2.0<br>0.0   | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990  | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387<br>0.935523<br>1.026131   | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190<br>3.050251   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397<br>1.016750  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>85C<br>257C<br>377C<br>al-Only  | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-4.0<br>-0.2<br>Actual   | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8<br>s and   | 1.0<br>2.0<br>2.0<br>0.0<br>-2.0<br>0.0<br><u>New E</u>   | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990<br>BellSouth Proj  | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387<br>0.935523<br>1.026131<br>ections  | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813<br>1.026131   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190<br>3.050251<br>2.884934   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397<br>1.016750  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>85C<br>257C<br>377C<br>al-Only<br>1C  | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-4.0<br>-0.2<br><b>Actual</b><br>-4.2  | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8<br><b>s and</b><br>0.3   | 1.0<br>2.0<br>2.0<br>0.0<br>-2.0<br>0.0<br><u>New E</u><br>0.6  | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990<br><b>kellSouth Proj</b><br>0.957746   | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387<br>0.935523<br>1.026131<br>ections<br>0.960712  | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813<br>1.026131   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190<br>3.050251<br>2.884934<br>2.884934   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397<br>1.016750<br>0.961645<br>0.962545  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>85C<br>257C<br>377C<br>al-Only<br>1C<br>22C                                     | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-4.0<br>-0.2<br><b>Actual</b><br>-4.2<br>-2.0  | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8<br><b>s and</b><br>0.3<br>0.3  | 1.0<br>2.0<br>2.0<br>-2.0<br>0.0<br><u>New E</u><br>0.6<br>-5.9   | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990<br>RellSouth Proj<br>0.957746<br>0.979744  | 1.012647<br>1.005806<br>1.016222<br>1.01208<br>0.998387<br>0.935523<br>1.026131<br>ections<br>0.960712<br>0.982942   | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813<br>1.026131<br>0.966476<br>0.924949   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190<br>3.050251<br>2.884934<br>2.887635<br>3.029453   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397<br>1.016750<br>0.961645<br>0.962545<br>1.009818  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>85C<br>257C<br>377C<br>al-Only<br>1C<br>22C<br>45C                              | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-0.2<br><b>Actual</b><br>-4.2<br>-2.0<br>2.3   | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8<br><b>s and</b><br>0.3<br>0.3<br>0.3   | 1.0<br>2.0<br>0.0<br>-2.0<br>0.0<br><u>New E</u><br>0.6<br>-5.9<br>-4.6                                 | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990<br><b>kellSouth Proj</b><br>0.957746<br>0.979744<br>1.023429   | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387<br>0.935523<br>1.026131<br>ections<br>0.960712<br>0.982942<br>1.026624  | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813<br>1.026131<br>0.966476<br>0.924949<br>0.979399   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190<br>3.050251<br>2.884934<br>2.887635<br>3.029453<br>3.207870   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397<br>1.016750<br>0.961645<br>0.962545<br>1.009818<br>1.069290  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>85C<br>257C<br>377C<br>al-Only<br>1C<br>22C<br>45C<br>4C                        | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-0.2<br><b>Actual</b><br>-4.2<br>-2.0<br>2.3<br>7.1  | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8<br><b>s and</b><br>0.3<br>0.3<br>0.3<br>1.8  | 1.0<br>2.0<br>0.0<br>-2.0<br>0.0<br><b>New E</b><br>0.6<br>-5.9<br>-4.6<br>-4.0                         | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990<br><b>bellSouth Proj</b><br>0.957746<br>0.979744<br>1.023429<br>1.071006                                     | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387<br>0.935523<br>1.026131<br>ections<br>0.960712<br>0.982942<br>1.026624<br>1.026624<br>1.090237  | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813<br>1.026131<br>0.966476<br>0.924949<br>0.979399<br>1.046627   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190<br>3.050251<br>2.884934<br>2.884934<br>2.887635<br>3.029453<br>3.029453<br>3.207870<br>2.854517   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.018749<br>0.995699<br>0.937397<br>1.016750<br>0.961645<br>0.962545<br>1.009818<br>1.069290<br>0.951506  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>85C<br>257C<br>377C<br>al-Only<br>1C<br>22C<br>45C<br>4C<br>52C                 | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-0.2<br><b>Actual</b><br>-4.2<br>-2.0<br>2.3<br>7.1<br>-2.9  | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8<br><b>s and</b><br>0.3<br>0.3<br>0.3<br>1.8<br>-0.1  | 1.0<br>2.0<br>0.0<br>-2.0<br>0.0<br><b>New E</b><br>0.6<br>-5.9<br>-4.6<br>-4.0<br>-5.7                 | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990<br><b>kellSouth Proj</b><br>0.957746<br>0.979744<br>1.023429<br>1.071006<br>0.970652                         | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387<br>0.935523<br>1.026131<br>ections<br>0.960712<br>0.982942<br>1.026624<br>1.090237<br>0.969565  | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813<br>1.026131<br>0.966476<br>0.924949<br>0.979399<br>1.046627<br>0.914300   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190<br>3.050251<br>2.884934<br>2.887635<br>3.029453<br>3.207870<br>2.854517<br>2.920351   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.018749<br>0.995699<br>0.937397<br>1.016750<br>0.961645<br>0.962545<br>1.009818<br>1.069290<br>0.951506<br>0.973450  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>257C<br>377C<br><b>al-Only</b><br>1C<br>22C<br>45C<br>4C<br>52C<br>5C           | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-4.0<br>-0.2<br><b>Actual</b><br>-4.2<br>-2.0<br>2.3<br>7.1<br>-2.9<br>-0.8  | 1.0<br>1.3<br>0.8<br>-2.5<br>2.8<br><b>s and</b><br>0.3<br>0.3<br>0.3<br>1.8<br>-0.1<br>0.1  | 1.0<br>2.0<br>0.0<br>-2.0<br>0.0<br><b>New E</b><br>0.6<br>-5.9<br>-4.6<br>-4.0<br>-5.7<br>-5.9         | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990<br><b>kellSouth Proj</b><br>0.957746<br>0.979744<br>1.023429<br>1.071006<br>0.970652<br>0.992248             | 1.012647<br>1.005806<br>1.016222<br>1.012081<br>0.998387<br>0.935523<br>1.026131<br>ections<br>0.960712<br>0.982942<br>1.026624<br>1.090237<br>0.969565<br>0.993355  | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813<br>1.026131<br>0.966476<br>0.924949<br>0.979399<br>1.046627<br>0.914300<br>0.934748   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>3.050251<br>2.884934<br>2.887635<br>3.029453<br>3.029453<br>3.029453<br>3.029453<br>2.8854517<br>2.920351<br>2.920351  | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397<br>1.016750<br>0.961645<br>0.962545<br>1.009818<br>1.069290<br>0.951506<br>0.973450<br>0.978850  |
| 52C<br>5C<br>822C<br>845C<br>852C<br>257C<br>377C<br>al-Only<br>1C<br>22C<br>45C<br>45C<br>45C<br>52C<br>52C<br>822C | 0.3<br>-0.4<br>0.3<br>-0.1<br>-1.0<br>-0.2<br><b>Actual</b><br>-4.2<br>-2.0<br>2.3<br>7.1<br>-2.9<br>-0.8<br>-2.1  | 1.0<br>1.3<br>1.3<br>0.8<br>-2.5<br>2.8<br><b>s and</b><br>0.3<br>0.3<br>0.3<br>1.8<br>-0.1<br>0.1<br>0.5  | 1.0<br>2.0<br>0.0<br>-2.0<br>0.0<br><b>New E</b><br>0.6<br>-5.9<br>-4.6<br>-4.0<br>-5.7<br>-5.9<br>-1.0 | 1.002710<br>0.995646<br>1.003476<br>0.998658<br>0.990323<br>0.959854<br>0.997990<br><b>BellSouth Proj</b><br>0.957746<br>0.979744<br>1.023429<br>1.071006<br>0.970652<br>0.992248<br>0.979021 | 1.012647<br>1.005806<br>1.016222<br>1.01208<br>0.998387<br>0.935523<br>1.026131<br>ections<br>0.960712<br>0.982942<br>1.026624<br>1.096056<br>0.993355<br>0.983683   | 1.002520<br>1.015864<br>1.036547<br>1.032322<br>0.998387<br>0.916813<br>1.026131<br>0.966476<br>0.924949<br>0.979399<br>1.046627<br>0.914300<br>0.934748<br>0.973846   | 3.017877<br>3.017315<br>3.056246<br>3.043060<br>2.987097<br>2.812190<br>3.050251<br>2.884934<br>2.887635<br>3.029453<br>3.207870<br>2.854517<br>2.920351<br>2.936550<br>2.936550   | 1.000907<br>1.005959<br>1.005772<br>1.018749<br>1.014353<br>0.995699<br>0.937397<br>1.016750<br>0.961645<br>0.962545<br>1.009818<br>1.069290  |
|  | 50<br>322C<br>322C<br>352C<br>355C<br>255C<br>255C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>377C<br>37 | 5C         5.0           322C         1.0           345C         2.0           352C         2.0           355C         2.0           355C         2.0           357C         2.0           357C         2.0           377C         1.0           3         2           1C         0.8           22C         -0.1           15C         1.5           4C         2.9           5C         -0.3           322C         -0.4           345C         0.3           35C         -0.1           35C         -0.1           35C         -0.1           35C         -0.2           35C         -0.2 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 5C         5.0         4.0         4.0         1.050000           322C         1.0         1.0         1.0         1.010000           345C         2.0         2.0         2.0         1.020000           352C         2.0         2.0         1.020000           352C         2.0         2.0         1.020000           35C         0.0         0.0         0.0         1.000000           257C         -2.0         0.0         0.0         9.80000           377C         1.0         1.0         1.0         1.010000           3         5.0         1.0         1.0         1.010000           3         1.0         1.0         1.0         1.010000           3         1.0         1.0         1.010000         3.0           3         1.0         1.0         1.010000         3.0           3         1.0         1.0         1.015451         4.0         0.993648           3         5.0         1.3         2.0         1.002710         3.22C         -0.4         1.0         1.0027470           3         1.0         4.0         1.003476         3.52C         -0.1         1.3 | 5C         5.0         4.0         4.0         1.050000         1.092000           322C         1.0         1.0         1.0         1.010000         1.020100           345C         2.0         2.0         2.0         1.020000         1.040400           352C         2.0         2.0         1.020000         1.040400           35C         0.0         0.0         0.0         1.000000         1.000000           35C         -2.0         0.0         0.0         0.980000         0.980000           377C         1.0         1.0         1.0         1.010000         1.020100           3         1.0         1.0         1.010000         1.022677           2C         -0.1         1.3         4.0         0.999127         1.0122677           3C         1.5         1.4         3.0         1.012647         1.022647           3C         0.3         1.0< | 5C         5.0         4.0         4.0         1.050000         1.092000         1.135680           322C         1.0         1.0         1.0         1.010000         1.020100         1.030301           345C         2.0         2.0         2.0         1.020000         1.040400         1.061208           352C         2.0         2.0         2.0         1.020000         1.040400         1.061208           35C         0.0         0.0         0.0         1.000000         1.000000         1.000000           257C         -2.0         0.0         0.0         9.80000         0.980000         0.980000           377C         1.0         1.0         1.010000         1.020100         1.030301           32         -         1.0         1.0         1.010000         1.020100         1.030301           32         -         1.0         1.0         1.010000         1.020100         1.030301           32         -         1.0         1.010000         1.022677         1.061193           22C         -0.1         1.3         4.0         0.999127         1.012227         1.052716           45C         1.5         1.4         3.0 | 5C         5.0         4.0         4.0         1.050000         1.092000         1.135680         3.277680           322C         1.0         1.0         1.0         1.010000         1.020100         1.030301         3.060401           345C         2.0         2.0         1.020000         1.040400         1.061208         3.121608           35C         2.0         2.0         1.020000         1.040400         1.061208         3.121608           35C         0.0         0.0         0.0         1.000000         1.000000         1.000000         3.000000           257C         -2.0         0.0         0.0         9.80000         0.980000         0.980000         2.940000           377C         1.0         1.0         1.010000         1.020100         1.030301         3.064010           322C         -0.1         1.3         4.0         0.999127         1.01227         1.052716         3.064070           35C         1.5         1.4         3.0         1.015451         1.029185         1.066060         3.104695           4C         2.9         2.0         3.5         1.029234         1.0439355         1.086447         3.165626           52C |

FLORIDA DOCKET 990649-TP · Minter DECLASSIFIED ATTACHMENT BFP-15 PAGE 3 OF 12

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**BellSouth Telecommunications** Forecast Telephone Plant Indexes Accounts On Part 32 USOA Basis

| FRC          | 1995                 | 1996         | 1997         | 1998         | 1999         | 2000         | 2001        | 2002        | 2003        | 2004        | 2005        | 2006         | 2007         | 2008+       | 1994 1995 1996 1997 1998 1999 2000 2001                 |
|--------------|----------------------|--------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|-------------|---|
| As Filed by  | RollSouth            |              |              |              |              |              |             |             |             |             |             |              |              |             |   |
| AS Flied by  | ACTUAL               | ACTUAL       | ACTUAL       |              |              |              |             |             |             |             |             |              |              |             |   |
| 1C           | ACTUAL<br>8.5        |              |              | 10           | 2.4          | 0.7          | 2.0         | 2.0         | 2.0         | 2.0         | 2.0         | 2.0          | 2.0          | 4.0         |   |
| 22C          |                      | 1.7          | 2.6          | 4.0          |              | 3.7          | 3.8         | 3.8         | 3.8         | 3.8         | 3.8         | 3.9          | 3.9          | 4.0         |   |
|              | 10.0                 | 2.2          | 1.8          | -1.0         |              | 4.0          | 4.0         | 4.0         | 4.0         | 3.0         | 3.0         | 4.0          | 4.0          | 4.0         |   |
| 45C          | 5.7                  | 2.0          | 3.0          | 1.0          |              | 4.0          | 3.0         | 3.0         | 3.0         | 3.0         | 3.0         | 4.0          | 4.0          | 3.0         |   |
| 4C           | 8.9                  | 1.3          | 2.2          | 1.5          |              | 3.2          | 3.7         | 3.5         | 3.4         | 3.4         | 3.4         | 3.5          | 3.5          | 3.0         |   |
| 52C          | 8.6                  | 3.1          | -2.1         | -3.0         |              | 5.0          | 4.0         | 4.0         | 3.0         | 3.0         | 3.0         | 3.0          | 3.0          | 3.0         |   |
| 5C           | 11.5                 | 1.7          | -0.2         | -2.0         | 0.0          | 5.0          | 4.0         | 4.0         | 3.0         | 3.0         | 3.0         | 3.0          | 4.0          | 3.0         |   |
| 822C         | -2.3                 | 1.2          | 0.8          | 1.0          | 1.0          | 1.0          | 1.0         | 1.0         | -1.0        | 1.0         | 1.0         | 2.0          | 2.0          | 2.0         |   |
| 845C         | 0.5                  | 2.1          | 1.5          | 2.0          | 2.0          | 2.0          | 2.0         | 2.0         | 1.0         | 2.0         | 2.0         | 3.0          | 3.0          | 2.0         |   |
| 852C         | -3.2                 | 1.6          | 1.7          | 1.0          | 1.0          | 2.0          | 2.0         | 2.0         | 1.0         | 2.0         | 2.0         | 2.0          | 3.0          | 2.0         |   |
| 85C          | -3.2                 | 0.9          | 0.1          | 0.0          | 0.0          | 0.0          | 0.0         | 0.0         | -2.0        | 0.0         | 1.0         | 1.0          | 1.0          | 1.0         |   |
| 257C         | -0.4                 | -2.0         | 1.1          | -3.0         | 0.0          | -2.0         | 0.0         | 0.0         | 0.0         | -1.0        | -2.0        | -2.0         | -2.0         | 0.0         |   |
| 377C         | 0.8                  | 10.5         | -0.4         | -2.0         | -1.0         | 1.0          | 1.0         | 1.0         | 2.0         | 0.0         | 0.0         | -1.0         | -1.0         | 1.0         |   |
| Updated Be   | South For            | Actuals      |              |              |              |              |             |             |             |             |             |              |              |             | Source: Attachment 2, Page 2-3                          |
|              | ACTUAL               | ACTUAL       | ACTUAL       | ACTUAL       | ACTUAL       | ACTUAL       | ACTUAL      |             |             |             |             |              |              |             |   |
| 1C           | 8.5                  | 1.7          | 2.6          | 2.5          | 1.6          | 0.8          | 1.5         | 3.8         | 3.8         | 3.8         | 3.8         | 3.9          | 3.9          | 4.0         | 131.3 134.6 136.7 137.8 139.8                           |
| 22C          | 10.0                 | 2.2          | 1.8          | -0.9         | -0.5         | -0.1         | 1.3         | 4.0         | 4.0         | 3.0         | 3.0         | 4.0          | 4.0          | 4.0         | 116.1 115.1 114.5 114.4 115.9                           |
| 45C          | 5.7                  | 2.0          | 3.0          | 0.2          |              | 1.5          | 1.4         | 3.0         | 3.0         | 3.0         | 3.0         | 4.0          | 4.0          | 3.0         | 115.6 115.8 116.5 118.3 119.9                           |
| 4C           | 8.9                  | 1.3          | 2.2          | 0.5          | 0.0          | 2.9          | 2.0         | 3.5         | 3.4         | 3.4         | 3.4         | 3.5          | 3.5          | 3.0         | 98.7 99.2 99.2 102.1 104.1                              |
| 52C          | 8.6                  | 3.1          | -2.1         | -1.0         |              | -0.6         | 1.1         | 4.0         | 3.0         | 3.0         | 3.0         | 3.0          | 3.0          | 3.0         | 110.8 109.7 110.2 109.5 110.7                           |
| 5C           | 11.5                 | 1.7          | -0.2         | -1.0         | 2.8          | 0.3          | 1.0         | 4.0         | 3.0         | 3.0         | 3.0         | 3.0          | 4.0          | 3.0         | 108.8 107.7 110.7 111.0 112.1                           |
| 822C         | -2.3                 | 1.2          | 0.8          | -4.7         | -5.9         | -0.4         | 1.0         | 1.0         | -1.0        | 1.0         | 1.0         | 2.0          | 2.0          | 2.0         | 76.8 73.2 68.9 68.6 69.3                                |
| 845C         | -2.5                 | 2.1          | 1.5          |              |              | -0.4         |             |             |             |             |             |              |              |             | 89.7 87.9 86.3 86.6 87.7                                |
|              |                      |              |              | -2.0         | -1.8         |              | 1.3         | 2.0         | 1.0         | 2.0         | 2.0         | 3.0          | 3.0          | 2.0         |   |
| 852C         | -3.2                 | 1.6          | 1.7          | -1.9         | -4.0         | -0.1         | 1.3         | 2.0         | 1.0         | 2.0         | 2.0         | 2.0          | 3.0          | 2.0         |   |
| 85C          | -3.2                 | 0.9          | 0.1          | -5.8         |              | -1.0         | 0.8         | 0.0         | -2.0        | 0.0         | 1.0         | 1.0          | 1.0          | 1.0         | 71.0 66.9 62.0 61.4 61.9                                |
| 257C<br>377C | -0.4<br>0.8          | -2.0<br>10,5 | 1.1<br>-0.4  | -1.1<br>-2.8 | -5.2<br>-4.6 | -4.0<br>-0.2 | -2.5<br>2.8 | 0.0<br>1.0  | 0.0<br>2.0  | -1.0<br>0.0 | -2.0<br>0.0 | -2.0<br>-1.0 | -2.0<br>-1.0 | 0.0<br>1.0  | 87.7 86.7 82.2 78.9 76.9<br>107.3 104.3 99.5 99.3 102.1 |
|              |                      |              |              |              |              | -0.2         |             |             |             |             | 0.0         | -1.0         | -1.0         | 1.0         | 101.0 104.0 55.0 55.0 102.1                             |
| Updated Be   | ISouth For<br>ACTUAL |              |              |              |              |              |             |             | tachment 3, |             | <b>DO D</b> | 50 p ·       | <b>DO D</b>  | D0 D        | Source: Attachment 2, Page 2-3                          |
| 10           |                      | ACTUAL       | ACTUAL       | ACTUAL       | ACTUAL       |              | ACTUAL      | BS Proj      | BS Proj      | BS Proj     |   |
| 1C           | 8.5                  | 1.7          | 2.6          | 2.5          |              | 0.8          | 1.5         | 2.5         | 2.7         | 3.1         | 2.9         | 3.0          | 3.9          | 3.6         | 131.3 134.6 136.7 137.8 139.8                           |
| 22C          | 10.0                 | 2.2          | 1.8          | -0.9         | -0.5         | -0.1         | 1.3         | 0.0         | 3.0         | 3.0         | 3.0         | 3.0          | 3.0          | 3.0         | 116.1 115.1 114.5 114.4 115.9                           |
| 45C          | 5.7                  | 2.0          | 3.0          | 0.2          | 0.6          | 1.5          | 1.4         | 1.0         | 3.0         | 3.0         | 3.0         | 3.0          | 3.0          | 3.0         | 115.6 115.8 116.5 118.3 119.9                           |
| 4C           | 8.9                  | 1.3          | 2.2          | 0.5          | 0.0          | 2.9          | 2.0         | 1.3         | 2.9         | 2.9         | 3.1         | 3.2          | 3.3          | 3.4         | 98.7 99.2 99.2 102.1 104.1                              |
| 52C          | 8.6                  | 3.1          | -2.1         | -1.0         | 0.5          | -0.6         | 1. <b>1</b> | 0.0         | 2.0         | 4.0         | 3.0         | 3.0          | 3.0          | 3.0         | 110.8 109.7 110.2 109.5 110.7                           |
| 5C           | 11.5                 | 1.7          | -0.2         | -1.0         | 2.8          | 0.3          | 1.0         | -1.0        | 2.0         | 4.0         | 3.0         | 3.0          | 3.0          | 3.0         | 108.8 107.7 110.7 111.0 112.1                           |
| 822C         | -2.3                 | 1.2          | 0.8          | -4.7         | -5.9         | -0.4         | 1.0         | 1.0         | 0.0         | 0.0         | 0.0         | -1.0         | 1.0          | 1.0         | 76.8 73.2 68.9 68.6 69.3                                |
| 845C         | 0.5                  | 2.1          | 1.5          | -2.0         | -1.8         | 0.3          | 1.3         | 2.0         | 1.0         | 2.0         | 2.0         | 2.0          | 2.0          | 3.0         | 89.7 87.9 86.3 86.6 87.7                                |
| 852C         | -3.2                 | 1.6          | 1.7          | -1.9         | -4.0         | -0.1         | 1.3         | 2.0         | 1.0         | 1.0         | 1.0         | 1.0          | 2.0          | 2.0         | 79.1 77.6 74.5 74.4 75.4                                |
| 85C          | -3.2                 | 0.9          | 0.1          | -5.8         | -7.3         | -1.0         | 0.8         | 0.0         | -2.0        | 0.0         | 1.0         | 1.0          | 1.0          | 1.0         | 71.0 66.9 62.0 61.4 61.9                                |
| 257C         | -0.4                 | -2.0         | 1.1          | -1.1         | -5.2         | -4.0         | -2.5        | -2.0        | 0.0         | -2.0        | 0.0         | -1.0         | 0.0          | 0.0         | 87.7 86.7 82.2 78.9 76.9                                |
| 377C         | 0.8                  | 10.5         | -0.4         | -2.8         | -4.6         | -0.2         | 2.8         | 0.0         | 0.0         | -2.0        | -2.0        | -1.0         | 0.0          | 0.0         | 107.3 104.3 99.5 99.3 102.1                             |
| Updated Be   | South For            | Material-On  | ly Actuals a | nd New Bell  | South Proje  | ctions       |             | Source: Att | tachment 3, | Page 5      |             |              |              |             | Source: Attachment 2, Page 4-6                          |
|              | ACTUAL               | ACTUAL       | ACTUAL       | ACTUAL       | ACTUAL       | ACTUAL       | ACTUAL      | BS Proj      | BS Proj      | BS Proj     |   |
| 1C           | 17.3                 | 0.0          | -0.2         | 0.7          | 0.0          | -4.2         | 0.3         | 0.6         | 0.6         | 2.4         | 0.6         | 0.6          | 4.2          | 1.9         | 114.5 134.3 134.3 134.0 134.9 134.9 129.2 129.6         |
| 22C          | 21.7                 | 1.7          | -1.0         | -5.6         | -2.9         | -2.0         | 0.3         | -5.9        | 0.8         | 4.0         | 2.5         | 2.0          | 2.0          | 2.4         | 83.5 101.6 103.3 102.3 96.6 93.8 91.9 92.2              |
| 45C          | 12.2                 | -0.9         | 1.7          | -5.6         | -2.1         | 2.3          | 0.3         | -4.6        | 1.2         | 3.2         | 2.3         | 1.9          | 1.8          | 2.1         | 89.8 100.8 99.9 101.6 95.9 93.9 96.1 96.4               |
| 400<br>40    | 13.5                 | -8.2         | -1.2         | -6.2         | -5.3         | 7.1          | 1.8         | -4.0        | 2.7         | 2.1         | 2.2         | 2.3          | 2.3          | 2.4         | 73.9 83.9 77.0 76.1 71.4 67.6 72.4 73.7                 |
| 52C          | 15.2                 | -0.2         | -1.2         | -6.2         | -5.5         | -2.9         | -0.1        | -5.7        | 0.8         | 4.0         | 2.5         | 2.0          | 2.0          | 2.4         | 86.6 99.8 103.0 97.2 91.2 92.0 89.3 89.2                |
| 52C          |                      |              |              |              | 4.0          | -2.9         | -0.1        |             | 1.0         | 4.0         | 2.5         | 2.0          | 2.0          | 2.4         | 75.9 94.5 95.0 90.8 86.8 90.3 89.6 89.7                 |
|              | 24.5                 | 0.5          | -4.4         | -4.4         |              |              |             | -5.9        | -3.0        |             | 2.5<br>-2.5 | -5.0         | -2.4<br>-2.5 | 2.0<br>-2.5 | 57.7 53.6 53.6 52.8 48.1 42.9 42.0 42.2                 |
| 822C         | -7.1                 | 0.0          | -1.5         | -8.9         | -10.8        | -2.1         | 0.5         | -1.0        |             | -2.5        |             |              |              |             |   |
| 845C         | -7.1                 | 0.0          | -1.5         | -8.9         | -10.8        | -2.1         | 0.5         | -1.0        | -3.0        | -2.5        | -2.5        | -5.0         | -2.5         | -2.5        | 57.7 53.6 53.6 52.8 48.1 42.9 42.0 42.2                 |

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#### CERTIFICATE OF SERVICE

I HEREBY CERTIFY that a true and correct copy of AT&T and MCI Joint Responses to FPSC Staff's Third Request for Production of Documents in Docket 990649A-TP has been served on the following parties by Hand Delivery (\*) and/or U. S. Mail this 4th day of March, 2002.

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